

Research Article

# Effect of Slotted holes on performance of Disc Brake

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## Abstract

The disc brake is a device for slowing or stopping the rotation of a wheel. Repetitive braking of the vehicle leads to heat generation during each braking event. Transient Thermal Analysis of the Rotor Disc of Disk Brake is aimed at evaluating the performance of disc brake rotor of a car under severe braking conditions and there by assist in disc rotor design and analysis. Disc brake model and analysis is done using ANSYS workbench 16.0. The main purpose of this study is to analysis the thermo mechanical behaviour of the dry contact of the brake disc during the braking phase. The coupled thermal-structural analysis is used to determine the thermal stresses and to calculate the Heat fluxes in x-y-z planes. This is established Slotted type and analysis is done by taking two different components such as Cast Iron and Stainless Steel and comparing which material is best suited for making of a disc brake.

**Keywords:** Disc brake, Thermal analysis, ANSYS workbench, Structural analysis.

## 1. Introduction

A disk brake consists of a cast iron disk bolted to the wheel hub and a stationary housing called caliper. The caliper is connected to some stationary part of the vehicle like the axle casing or the stub axle as is cast in two parts each part containing a piston. In between each piston and the disk there is a friction pad held in position by retaining pins, spring plates etc. passages are drilled in the caliper for the fluid to enter or leave each housing. The passages are also connected to another one for bleeding. Each cylinder contains rubber-sealing ring between the cylinder and piston. Disk brake types: 1. Drilled type 2. Drilled and slotted. 3. Disk with internally slotted.

Nevertheless, they are certain issues arising in the disc brakes while braking. Some of the issues which generally occur while braking are: NVH and Thermal issues.

### NVH Issues

Noise, vibration and harshness are complex issues that involve the entire system of components from the brake system. Ongoing investigations in the industry have identified several initiating factors relating to the brake elements themselves which can be grouped into the following sections:

- 1.Brake disc hot spots which typically result in thermal judder.
2. Uneven rotor thickness wear and rotor thickness variation.

### 3. Rotor deflection and oscillation.

#### Thermal management issues

1. Uneven heating of brake rotors can temporarily cause, or increase, thickness variation, and sometimes can produce a primary thermal buckling that warps the rotor.
2. Uneven rotor cooling in the case of a vehicle parked immediately following strenuous braking activity can cause the area of rotor under the brake pads to cool more slowly than the portion of the rotor open to the atmosphere, resulting in uneven thermal stresses in the rotor and leading to pad imprinting, residual internal stresses and material failure.

#### Objective

The main objectives in this work are:

1. To perform the thermal analysis on the disc brakes and to determine the thermal stresses, and to calculate the corresponding Heat flux of the disc brake by taking boundary conditions.
2. Evaluating the performance of individual disc brake under certain braking conditions.
3. Choosing the best possible material from the given materials under the required conditions.

## 2. Literature

Investigations performed to know the temperature fields of the solid disc brake during short, emergency braking. Transient thermal analysis of disc brakes in

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single brake application was performed. To obtain the numerical simulation parabolic heat conduction equation for two dimensional model was used. The results show that both evolution of rotating speed of disc and contact pressure with specific material properties intensely. In basic working operation, a disc or drum brake system has to reduce wheel speed when a driver desires vehicle deceleration. The kinetic energy generated by a vehicle in terms of wheel speed is converted into heat energy due to the application of the brake system. The friction force between disc/drum and brake pad/brake shoe applies friction torque to the wheel in the opposite direction of the car's movement. This result in the reduction of vehicle speed and heat energy occurring in the brake disc/drum causes a temperature increment in the disc/drum swept area during the brake application. This physical action of the brake disc/drum causes heat conduction to the adjacent braking system components (S. Lakkam *et al*, 2013), (K. Lee, 1999). The inconsistent dissipation of heat inside the brake disc could cause deformation of the disc. Even worst, the disc deformation could also cause friction loss and consequently led to brake fade (G. Cueva *et al*, 2013). Furthermore, high temperatures of the brake disc could cause cracking in the brake disc material due to high thermal stresses. On top of that these factors also cause vibration (F. Bergman *et al*, 1999, A. Papinniemia *et al*, 2002). It is become common in the brake research community to fully utilize finite element approach in order to identify and predict disc/drum brake structural performance. For instance, the physical shape of vehicle brake discs play a significant role in determining the temperature characteristics including the overall brake efficiency (S. Koetniyom, 2003).

There is a link interaction between mechanical and thermal effects with disc movements and heat caused by frictions. They concluded that, from finite element analysis, temperatures on the disc surface changed at each point over the period, which indicates inconsistent dissipation and temperature differences in each side of the disc. Hence, inconsistent contact between disc and pad could affect material deformation (Kamnerdtong *et al*, 2005). The finite element Software ANSYS study for the thermal behaviour of the dry contact between the discs of brake pads at the time of braking phase. Temperature distribution obtained by the transient thermal analysis was used in the calculations of the stresses on disc surface (Belhocine *et al*, 2014). Finite element method was used to calculate the heat generated on the surfaces of friction clutch and temperature distribution for case of bands contact between flywheel and clutch disc, and between the clutch disc and pressure plate (one bad central and two bands) and compared with case of full contact between surfaces for single engagement and repeated engagements (Abdullah *et al*, 2013). In other work, the finite element method used to study the contact pressure and stresses during the full engagement period of the clutches using

different contact algorithms. Moreover, sensitivity study for the contact pressure was presented to indicate the importance of the contact stiffness between contact surfaces (Abdullah *et al*, 2013). The effect of sliding speed on contact pressure distribution, temperature and heat flux generated along the frictional surfaces was analyzed. A static structural analysis of the disc brake whose some composite materials were selected to compare the results obtained such as deflection and stresses (Sowjanya *et al*, 2013). Thermal and structural coupled analysis was carried out to find the strength of the disc brake in the research (Reddy *et al*, 2013).

### 3. Materials and Methods

#### 3.1 Materials used for the disc brake

The Disc brake discs are commonly manufactured out of grey cast iron. The SAE maintains a specification for the manufacture of grey iron for various applications. For normal car and light truck applications, the SAE specification is J431 G3000 (superseded to G10). This specification dictates the correct range of hardness, chemical composition, tensile strength, and other properties necessary for the intended use. Some racing cars and airplanes use brakes with carbon fiber discs and carbon fiber pads to reduce weight. Wear rates tend to be high, and braking may be poor or grabby until the brake is hot. The materials used for rotor disc are explained in detail. It is investigating the temperature distribution, the thermal deformation, and the thermal stress of automotive brake disks have quite close relations with car safety; therefore, much research in this field has been performed.

#### 3.2 Modelling

The disc brakes created using Solid works 2016 in which main modules are:

- 1) Sketcher
- 2) Part
- 3) Assembly

Sketcher is used to create design and part is used to apply extrude and material to see the model in Three-Dimensional as shown in Fig.1 and 2.



**Fig.1** Slotted Disc Brake

After Modelling of the disc brakes, the thermal analysis of the disc brakes are done in Ansys workbench 16.0.

### 3.3 Thermal analysis

For analysis the following assumption have been made Assumptions:

- Brake is applied on the front wheel only.
- The analysis is based on pure thermal loading. The analysis does not determine the life of the disc brake.
- The kinetic energy of the vehicle is lost through the brake discs i.e. no heat loss between the tyres and the road surface and the deceleration is uniform.
- The disc brake model used is of homogenous material.
- The thermal conductivity of the material used for the analysis is uniform throughout.

#### Material properties

NOTE: The specific heat of the material used is constant throughout and does not change with the temperature.

Material: Cast iron

**Table 1** Cast iron Properties

S.no	Property	Value	Units
1	Density	7200	Kgm <sup>-3</sup>
2	Youngs Modulus	1.1E+11	Pa
3	Poissons Ratio	0.28	
4	Bulk Modulus	8.3333E+10	Pa
5	Shear Modulus	4.2969E+10	Pa
6	Ultimate tensile strength	2.4E+08	Pa
7	Ultimate compressive strength	8.2E+08	Pa
8	Isotopic thermal conductivity	52	Wm <sup>-1</sup> C <sup>-1</sup>

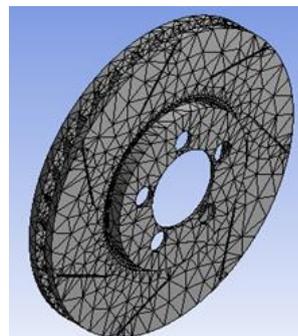
Material: Stainless Steel

**Table 2** Stainless Steel Properties

S.no	Property	Value	Units
1	Density	7750	Kgm <sup>-3</sup>
2	Youngs Modulus	1.93E+11	Pa
3	Poissons Ratio	0.31	
4	Bulk Modulus	1.693E+11	Pa
5	Shear Modulus	7.3664E+10	Pa
6	Tensile Yield strength	2.07E+08	Pa
7	Compressive Yield strength	2.07E+08	Pa
8	Tensile Ultimate strength	5.86E+08	Pa
9	Isotropic Thermal conductivity	15.1	Wm <sup>-1</sup> C <sup>-1</sup>

The goal of meshing in Workbench is to provide robust, easy to use meshing tools that will simplify the mesh generation process. The model using must be divided into a number of small pieces known as finite elements.

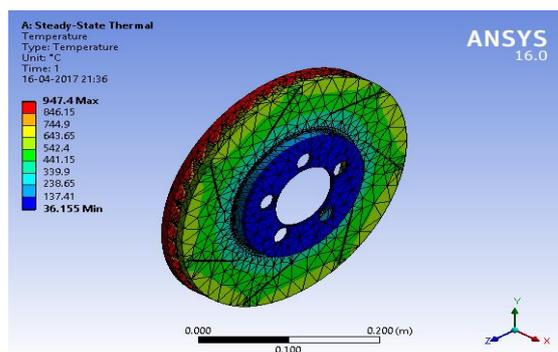
Since the model is divided into a number of discrete parts, in simple terms, a mathematical net or "mesh" is required to carry out a finite element analysis. A finite element mesh model generated is shown below with elements of 18768 and nodes of 33534.



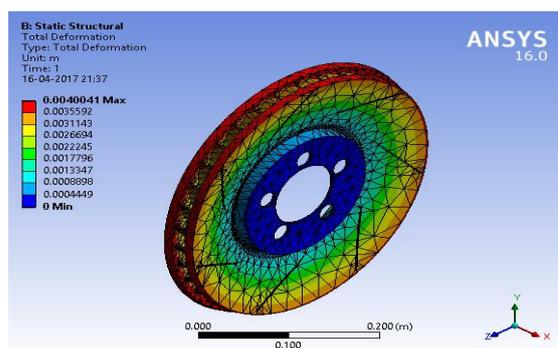
## 4. Results and discussion

The above figures showed that in slotted disc the redzones occur at the the edge of the rotor disc which is due to frictional force by the brake calliper. Since there is no drill holes in this type of design the convection of heat is less and hence the temperature is max compared to slotted and drilled disc brake. The maximum temperature for this disc is 947.4°C in using stainless steel as material and for cast iron it is 630.18 °C

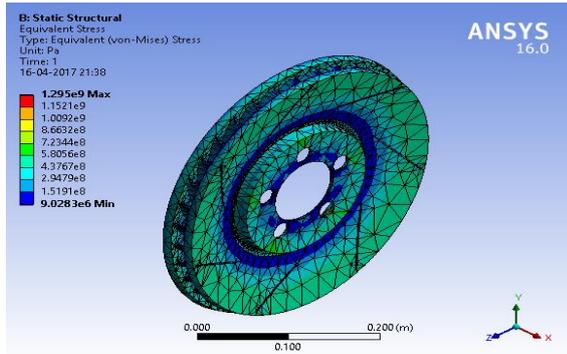
### 4.1 Slotted disc brake using stainless steel



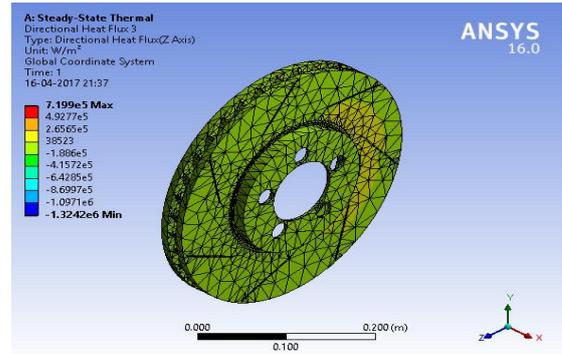
**Fig.2** Nodal Temperature  
Max= 947.4, Min = 36.155



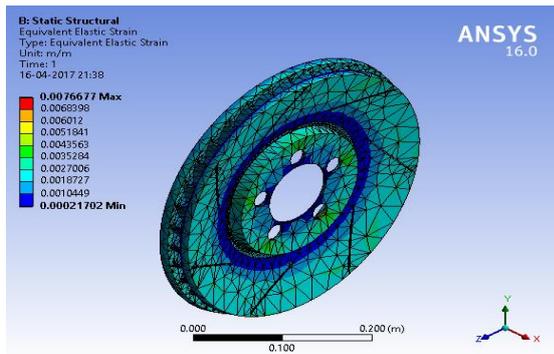
**Fig.3** Total Deformation (in m)  
Max = 0.0040041, Min = 0



**Fig.4** Equivalent Stress  
Max = 1.295e9, Min= 9.0283e6

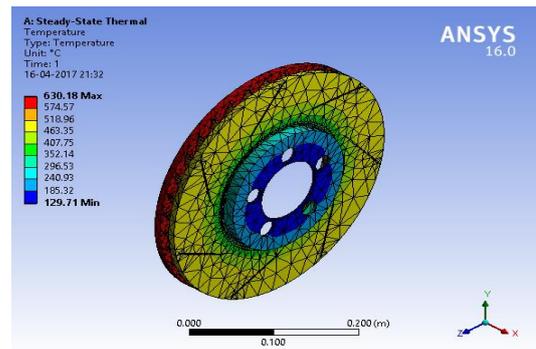


**Fig.8** Heat Flux (z-axis in W/m<sup>2</sup>)  
Max= 7.199e5, Min = -1.3242e6.

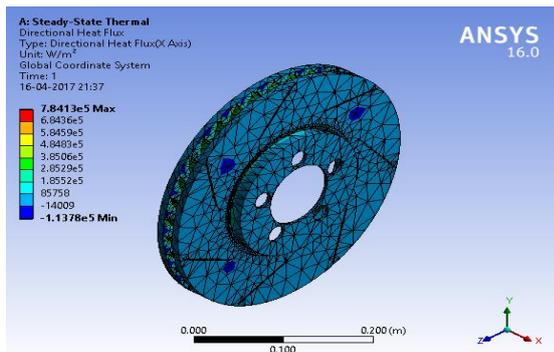


**Fig.5** Equivalent Strain( in m/m)  
Max= 0.0076677, Min= 0.00021702

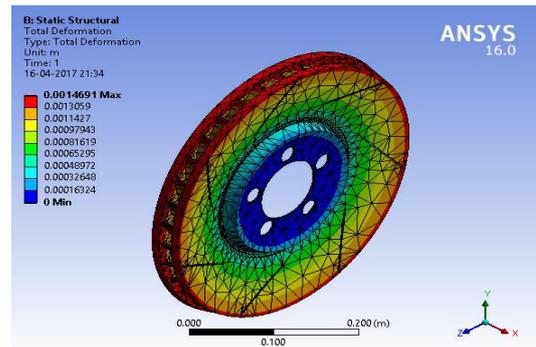
4.2 Slotted disc brake using cast iron



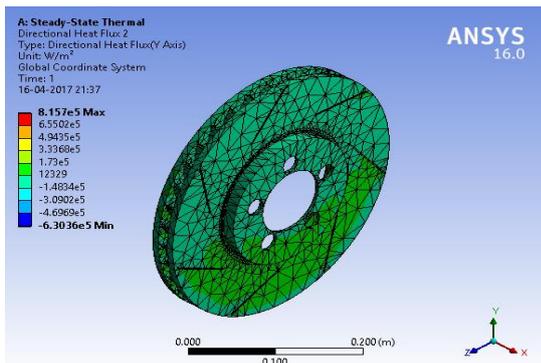
**Fig.9** Steady State Thermal Temperature (in degrees)  
Max =630.18, Min = 129.71



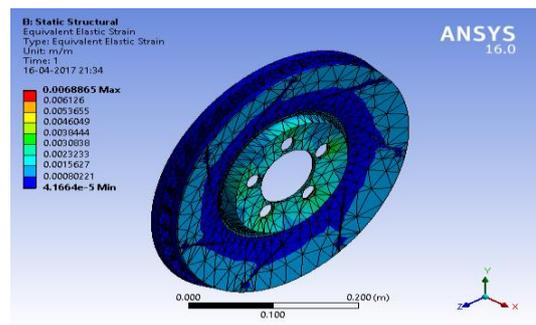
**Fig.6** Heat Flux on (x-axis in W/m<sup>2</sup>)  
Max= 7.8413e5, Min= -1.378e5



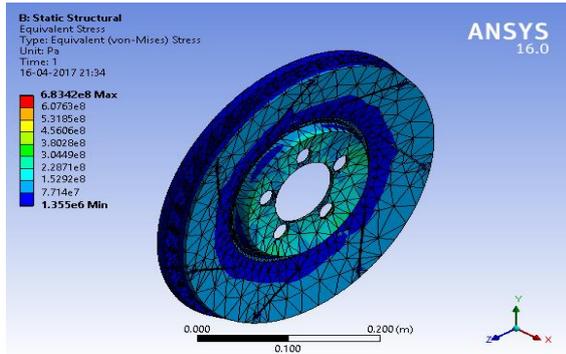
**Fig.10** Total Deformation (in m)  
Max= 0.0014691, Min = 0



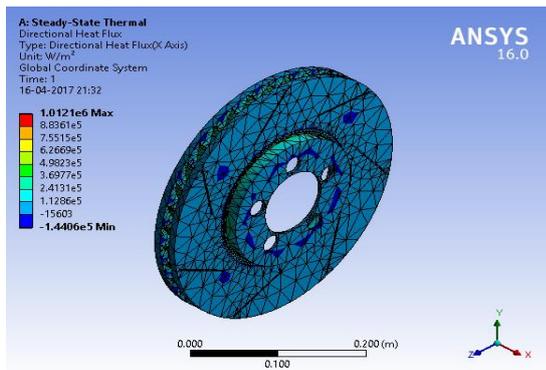
**Fig.7** Heat Flux(Y-axis in W/m<sup>2</sup>)  
Max= 8.157e5, Min = -6.3036e5



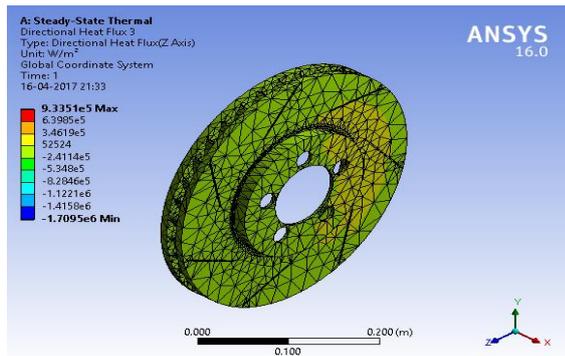
**Fig.11** Equivalent Strain (in m/m)  
Max= 0.0068865, Min= 0.00041664



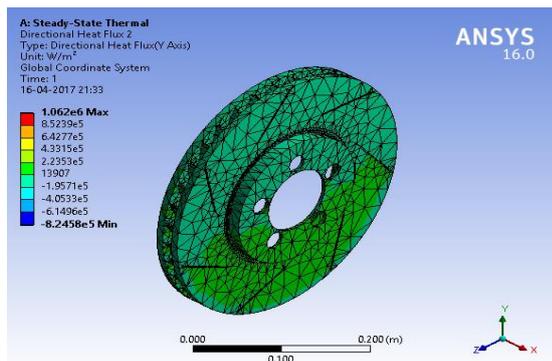
**Fig.12** Equivalent Stress (von – mises in Pa)  
Max = 6.8e8, Min = 1.33e6



**Fig.13** Heat Flux(X-axis in W/m<sup>2</sup>)  
Max = 1.012e6, Min = -1.44e5



**Fig.14** Heat Flux (Z-axis in W/m<sup>2</sup>)  
Max = 9.33e5, Min = -1.709e6



**Fig.15** Heat Flux(Y-axis in W/m<sup>2</sup>)  
Max = 1.062e6, Min = -8.24e5

**Table 3** Comparison of CI and SS slotted disc

Type Of Material	Thermal Temperature(°C)		Thermal Deformation(m)	
	Max.	Min.	Max.	Min.
Caste Iron	630.18	129.17	0.0014691	0
Stainless Steel	947.4	36.155	0.0040041	0

**Conclusions**

Comparing the different results obtained from the analysis, it is concluded that Cast Iron is the best material for both slotted disc, because the thermal temperature and thermal stresses obtained for this material is lesser than compared to the stainless steel material.

- CI disc showed 33% reduction in temperature
- Deformation was less in CI by 75% compared to SS

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