

Research Article

# Designing of Cement Slurry to Enhance Compressive Strength and Rheology: An Experimental Study

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## Abstract

The most essential function of oil and gas well cement is to provide isolation of zones in a production well. Cement isolates the wellbore in completion of oil and gas wells, prevents failure of casing, and it also prevents wellbore fluids so that they cannot be contaminated from fresh water aquifers. In slurry state cement is distinguished by rheological properties like plastic viscosity and yield stress. Proper selection of cement slurries plays a vital role in well cementing and that could be possible with the utilization of efficient materials that may result the superior rheological properties of cement slurry i.e. plastic viscosity, gel and yield strength. The selection of cement has been done on account of higher values of compressive strengths for which quality of cement sheath will be enhanced. Cement Slurry design can be optimized by operators for which it is mandatory for operators that they have knowledge about actual temperature that cement will encounter inside wellbore. Down hole temperatures of cementing have impact on thickening time, rheology, and compressive strength development. In this research work Rice Husk Ash (RHA) and Egg Shell Powder (ESP) are used in cement slurry so that compressive strength of cement specimen can be increased. The cement slurry has been made from locally manufactured cement, water, RHA and ESP. Cement slurry of 600ml by volume has been prepared. Specimens with size of 2×2×2 inch cubic molds are made for compressive strength testing at different curing conditions. Three variants of the specimen with varying concentrations of RHA and ESP are made. In present work during slurry state the rheological properties are determined while in solid state compressive strength of cement specimen at three curing ages of 08 hours, 24 hours and 72 hours is determined.

**Keywords:** Compressive strength, Rheological properties, well bore fluids, plastic viscosity, thickening time, cubic mold and curing ages.

## 1. Introduction

Oil well cementing has been played a vital part in producing the hydrocarbons from subsurface to surface successfully. In oil and gas well completion, cement isolates the wellbore, prevents casing failure and to form a competent hydraulic seal during the whole operational lifetime of the well for long-term zonal isolation (Parcevaux, P. A., and P. H. Sault, 1984). The stresses inside the wellbore get increased and resultant cement sheath integrity damaged because of rock movement (Erik B. Nelson and Dominique Guillot, 2006).

The down hole environment (temperature, pressure, formation water chemistry) will govern the design of the cement slurry and impact on the performance across the full lifecycle of a well.

The density and rheological properties will determine the success of the initial placement of the cement (Anna Piłkowska, 2017).

During the operational life, variations in temperature and pressure will occur. Knowledge of the behavior of the set cement material due to the curing temperature and pressure and there after changes in the material response (stiffness, ductility etc) owing to changes in temperature and applied stresses, including fatigue degradation due to loading cycles, is vital in ensuring the reliability of well designs (Heinold, *et al*, 2002).

Additives like RHA and ESP are mixed in cement slurry in order to increase compressive strength of cement sheath during cementing of oil well where there are high pressures and high temperatures concerned. Cement selection is based on the high values of compressive strength and as an outcome cement of improved quality will be obtained.

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### 1.1 Compressive Strength

The compressive strength is played vital importance and has tested the accuracy of oil well cementing and has capability to resist distortion when load has been applied. In general, the compressive strength increases with increase in curing time. The hydration is reaction between cement particles. The hydration has been accelerated with available of evaporated water (Falode OA, *et al*, 2013).

All tests related to compressive strength can be preceded before cementing job by Service Company. Cement compressive strength relies on additives used, mix designs, time of curing and exposure conditions. When cement gets set, it possesses compressive strength with passage of time. The compressive strength has produced in cement may be dependent on time, temperature, and pressure.

## 2. Research Methodology

This research project has been carried out to detect cement with maximum compressive strength and optimum rheological properties. In order to examine it, we have prepared cement samples with locally manufactured cement with addition of ESP and RHA with various concentrations.

### 2.1 Selection of Additives

In this project two additives are selected which enhance both rheological and mechanical properties of cement.

#### 2.11 Eggshell powder (ESP)

Egg shells are obtained from nearby hotels and hostels of Jamshoro. Egg shell powder is obtained from egg shells. Due to present of  $\text{CaCO}_3$  in ESP, it increases compressive strength of cement.

U.N Okonkwo, *et al* (2012) it's scientifically believed that eggshell is principally made of compounds of calcium carbonate ( $\text{CaCO}_3$ ) which is 93.7% of overall composition of the eggshell. Similarly, in production of cement calcium carbonate ( $\text{CaCO}_3$ ) is primary material.

#### 2.12 Rice Husk Ash (RHA)

Rice husks are also obtained from rice mills nearby Jamshoro. Rice husk ash is formed from rice husk in incineration furnace. About 80-85% of silica is contained in RHA. RHA increases compressive strength of cement when specific amount of RHA is added into the slurry.

### 2.2 Materials and Specimen

Cement slurry was prepared from locally manufactured cement, water, RHA and ESP. Cement

slurry of 600 ml by volume is prepared. The water is added to cement within limits of 50% to 66% bwoc. Specimens with size of 2×2×2 inch cubic molds are made for compressive strength testing. Three variants of the specimen are made in this study.

### 2.3 Experimental Work

The experiments are performed in laboratory on locally manufactured cement slurry to examine potential of locally manufactured cement mixed with oil well cement additives at test conditions of 90°C temperature and 20 MPa pressure. The cement slurry and preparation of specimen are carried out by closely following American Petroleum Institute (API) Specification 10A.

The specific quantity of every material has been weighted with electronic balance. The chosen amount of RHA has been added to water in cement blender at 1600 rpm, after 20 seconds, ESP mixed in cement slurry and it has been blended again for 20 seconds.

#### 2.3.1 Plastic Viscosity and Gel strength

In slurry state rheological properties are determined. The fundamental reason to determine rheological properties is to forecast flow characteristics of cement slurry using Plastic Viscosity and Gel Strength. Slurry is preconditioned in consistometer before placing it in viscometer. Once preconditioning is completed, preheated cup of viscometer is filled by slurry and the test begins at desired temperature. Dial readings at six speeds i-e 600 rpm, 300 rpm, 200 rpm, 100 rpm, 6 rpm and 3 rpm are noted to calculate plastic viscosity. It is calculated by subtracting the reading at 600 rpm from the reading at 300 rpm. Gel strength is calculated at 10 seconds and 10 minutes.

#### 2.3.2 Thickening Time Test

The HPHT Consistometer is used to determine the thickening time of the cement slurries at well bore temperature 90°C temperature and 20 MPa pressure. When BC value reaches 30 means the slurry loses its pump-ability. When its BC values reaches 70 or 100 means slurry has got thick.

#### 2.3.3 Measurement of Slurry Density

After cement slurry has been prepared, there is dire need to verify its density either it is up to our need or target or not. While measuring the slurry density, we use the mud balance at a laboratory.

#### 2.3.4 Compressive Strength Test

In hardened state compressive strength of cement is determined. The wet mix is then poured into 2×2×2 inch cubic molds and kept for 24 hours. Afterwards they are demoulded and kept for water curing for 08,

24 and 72 hours. Once samples have achieved specified curing at curing conditions of 90°C temperature and 20 MPa, pressure physical properties are examined by following API Specification 10A and API Recommended Practice 10B. The cubic molds of cement are tested in universal testing machine for compressive strength test.

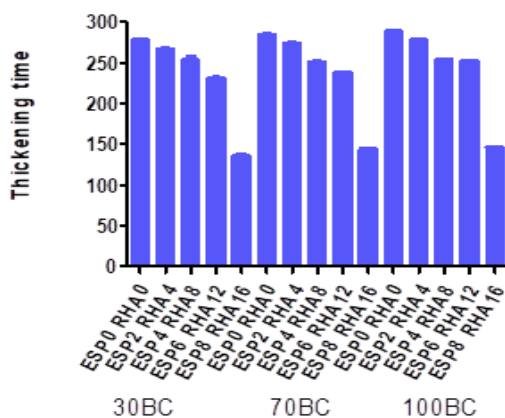
### 3. Results and Discussions

#### 3.1 Thickening Time

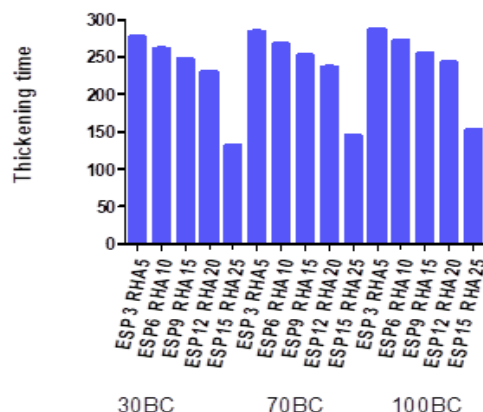
Results are determined by making 15 variants of cement slurry and in each variant five samples of cement slurry are tested in order to get average value of each test. ESP and RHA have accelerating effect therefore thickening times are getting decreased by increasing concentration of both additives. Results of thickening time tests are given in the Table No: 1

**Table 1** Determination of thickening time with following ESP and RHA concentration.

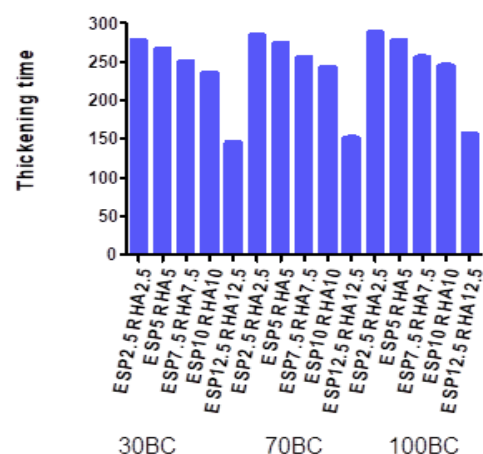
Cement Slurry (ml)	ESP %	RHA %	Test condition °C×Mpa×min	Thickening time (min)		
				30 Bc	70 Bc	100 Bc
600	0	0	90x20x85	278	285	288
600	02	4	90x20x85	267	274	278
600	04	8	90x20x85	253	251	253
600	06	12	90x20x85	231	238	252
600	08	16	90x20x85	136	144	146
600	2.5	2.5	90x20x85	278	285	288
600	5	5	90x20x85	267	274	278
600	7.5	7.5	90x20x85	251	255	257
600	10	10	90x20x85	236	243	246
600	12.5	12.5	90x20x85	146	152	156
600	3	5	90x20x85	278	285	288
600	6	10	90x20x85	262	268	272
600	9	15	90x20x85	248	253	256
600	12	20	90x20x85	230	237	244
600	15	25	90x20x85	132	146	153



**Fig: 1** Graph shows thickening time at 0 to 8% ESP & 0 to 16% RHA



**Fig: 2** Graph shows thickening time with 2.5% to 12.5% ESP & 2.5 to 12.5 %RHA



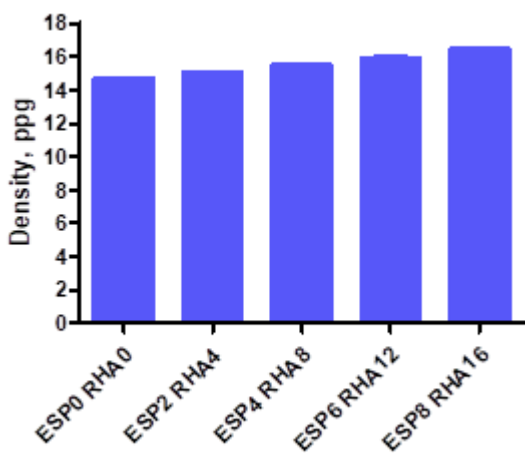
**Fig: 3** Graph shows slurry thickening time with 3 to 15% ESP & 5 to 25 % RHA

#### 3.2 Slurry density and Plastic Viscosity

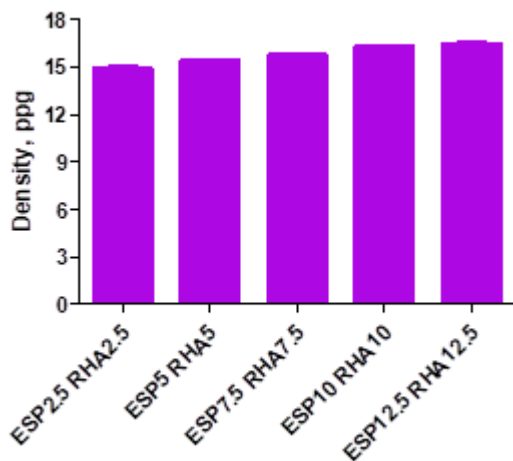
Slurry density is determined by using mud balance. Plastic viscosity is determined using Rotational viscometer by taking dial readings at 6 speeds i-e 600 , 300, 200, 100, 6 and 3 rpm. Plastic obtained by: 600 rpm reading- 300 rpm reading. At concentration of ESP 15% and RHA 25% density obtained is 17.52 ppg which is higher than rest of all concentrations used shown in fig 08. But it is lowest 14.66 ppg with ESP 0% & RHA 0% shown in fig: 04. Slurry density is decreased with increasing the concentration of both additives. Values of densities of all cement slurries obtained between 14-17 ppg that are according to API specification and recommended practice 10B. Plastic viscosity is maximum i-e 67.2 cP with ESP 7.5% & RHA 7.5%. Whereas it is minimum with sample having ESP 10% and RHA 10% shown in fig: 07. The values of plastic viscosity of all cement slurries are below 100 cP that is according to (Abbas et al, 2014) is favorable to retain cement slurry being pumpable. Test results of both Density and plastic viscosity are given in the Table no: 02.

**Table 2** Determination of slurry density & Plastic Viscosity with following ESP & RHA concentration.

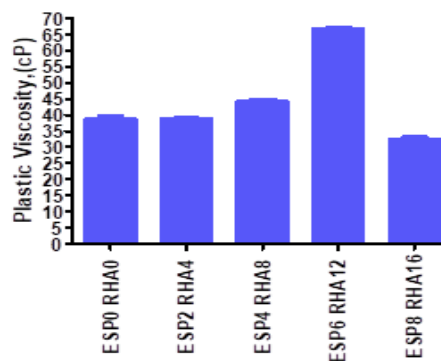
Cement Slurry (ml)	ESP %	RHA %	Test condition	Slurry density (ppg)	Plastic viscosity (cP)
			°C×Mpa		
600	0	0	90x20	14.66	39
600	02	4	90x20	15.06	38.8
600	04	8	90x20	15.52	44.4
600	06	12	90x20	15.92	66.8
600	08	16	90x20	16.44	32.6
600	2.5	2.5	90x20	14.92	39
600	5	5	90x20	15.38	43.8
600	7.5	7.5	90x20	15.76	67.2
600	10	10	90x20	16.26	29
600	12.5	12.5	90x20	16.46	33
600	3	5	90x20	15.18	39.8
600	6	10	90x20	15.64	45.2
600	9	15	90x20	16.24	65.8
600	12	20	90x20	16.94	29.2
600	15	25	90x20	17.52	30.4



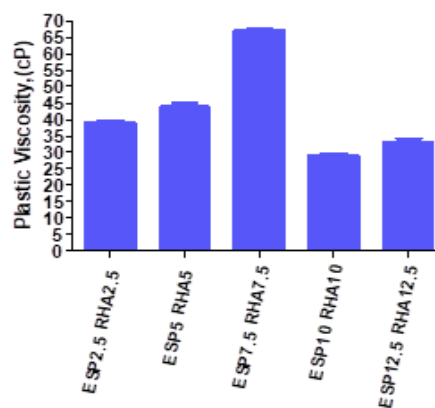
**Fig: 4** Graph shows slurry density at 0 to 8% ESP & 0 to 16 %RHA



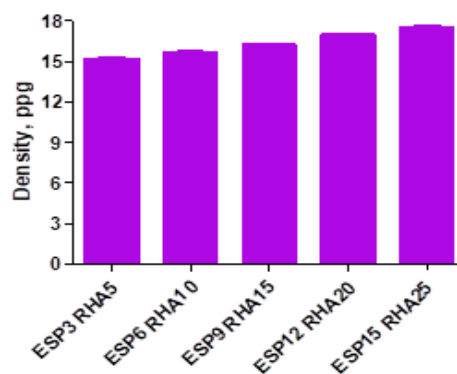
**Fig: 5** Graph shows plastic viscosity at 0 to 8% ESP & 0 to 16 % RHA



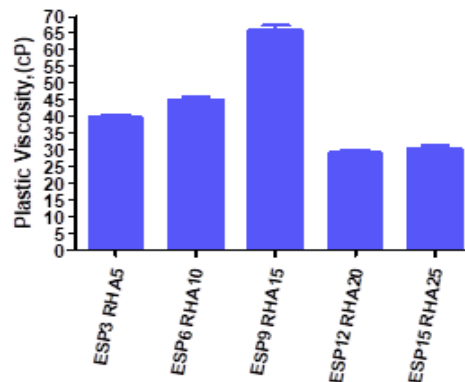
**Fig: 6** Graph shows density at 2.5 to 12.5% ESP & 2.5 to 12.5 %RHA



**Fig: 7** Graph shows plastic viscosity at 2.5 to 12.5% ESP & 2.5 to 12.5 %RHA



**Fig: 8** Graph shows density at 3 to 15% ESP & 5 to 25 % RHA



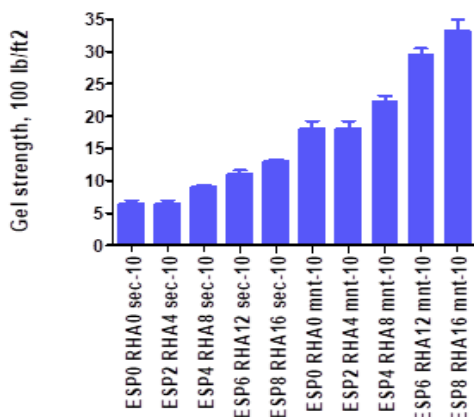
**Fig: 9** Graph shows plastic viscosity at 3 to 15% ESP & 5 to 25% RHA

### 3.3 Gel Strength

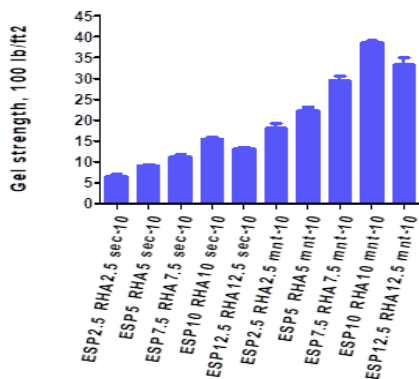
Minimum Gel strength 6.2 and 18 lb/100 ft<sup>2</sup> with slurry having ESP0% & RHA0% at 10 seconds and 10 minutes respectively shown in fig: 10. Maximum gel strength 15.4 lb/ 100 ft<sup>2</sup> and 38.7 lb/ 100 ft<sup>2</sup> obtained with slurry having ESP 10% & RHA 10 at 10 seconds and 10 minutes respectively as shown in fig 11. In Table No: 03 concentrations of RHA and ESP and results obtained on these concentrations are given.

**Table 03** Determination of Gel strength with following ESP & RHA concentration

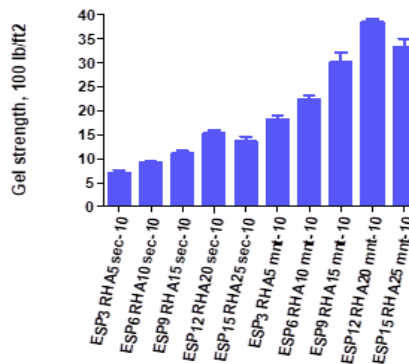
Cement Slurry (ml)	ESP %	RHA %	Test condition °C×Mpa	Gel Strength lb/100 ft <sup>2</sup>	
				10 Sec	10 min
600	0	0	90x20	6.2	18
600	02	4	90x20	6.3	18.1
600	04	8	90x20	9.0	22.3
600	06	12	90x20	11.1	29.4
600	08	16	90x20	13.1	33.3
600	2.5	2.5	90x20	6.4	18.2
600	5	5	90x20	9	22.3
600	7.5	7.5	90x20	11.1	29.4
600	10	10	90x20	15.4	38.7
600	12.5	12.5	90x20	13.1	33.4
600	3	5	90x20	7	18.3
600	6	10	90x20	9.1	22.3
600	9	15	90x20	11.1	30
600	12	20	90x20	15.3	38.5
600	15	25	90x20	13.7	33.5



**Fig: 10** Graph shows gel strength at 0 to 8% ESP & 0 to 16 % RHA



**Fig: 11** Graph shows gel strength at 2.5 to 12.5% ESP & 2.5 to 12.5 %RHA



**Fig: 12** Graph shows gel strength with 3 to 15% ESP & 5 to 25 %RHA

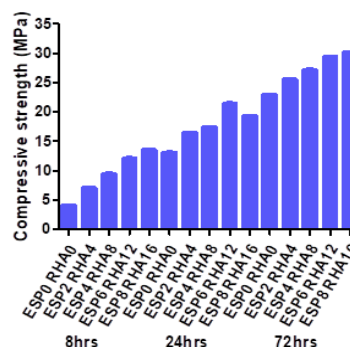
### 3.4 Compressive Strength

The sample with ESP 10% and RHA10% showed high value of CS 30.16 MPa at curing period of 72 hours. At curing period of 24 hours with same ESP & RHA% the value of CS obtained is 20.44 MPa. While at the curing period of 08 hours, the value of CS is 14.10 MPa which is lower than curing periods of 24 hours and 72 hours shown in fig: 14.

The sample with ESP 0% and RHA0% showed lowest value of CS 23.02 Mpa, 13.18 Mpa and 4.16 MPa at curing period of 72 hours, 24 hours and 08 hours respectively shown in fig: 13.

**Table 04** Determination of Compressive strength with following ESP & RHA concentration.

Cement Slurry (ml)	ESP %	RHA %	Test condition °×Mpa	Compressive Strength (MPa)		
				8 hrs	24 hrs	72 hrs
600	0	0	90x20	4.16	13.18	23.02
600	02	4	90x20	7.14	16.52	25.56
600	04	8	90x20	9.56	17.50	27.26
600	06	12	90x20	12.18	21.50	29.46
600	08	16	90x20	13.58	19.34	30.16
600	2.5	2.5	90x20	6.86	15.04	24.20
600	5	5	90x20	9.08	17.52	25.60
600	7.5	7.5	90x20	11.14	18.72	26.30
600	10	10	90x20	14.10	20.44	31.32
600	12.5	12.5	90x20	12.12	19.80	29.54
600	3	5	90x20	8.46	16.26	26.16
600	6	10	90x20	9.12	16.82	26.74
600	9	15	90x20	13.06	19.60	29.84
600	12	20	90x20	11.28	17.84	28.12
600	15	25	90x20	9.20	15.80	25.28



**Fig: 13** Graph shows CS at 0 to 8% ESP & 0 to 16 %RHA



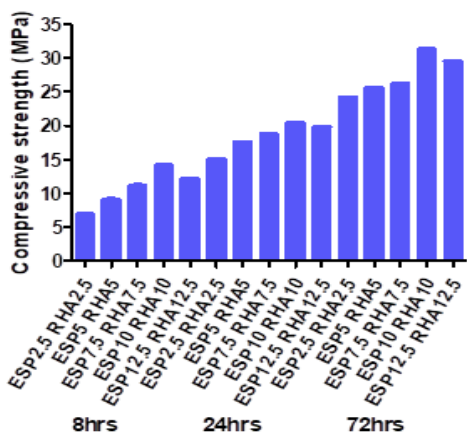


Fig: 14 Graph shows CS at 2.5 to 12.5% ESP & 2.5 to 12.5 % RHA

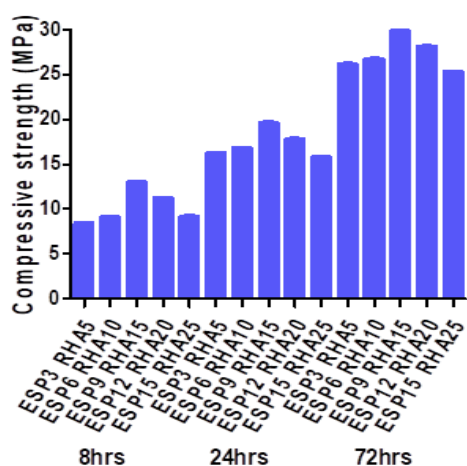


Fig: 15 Graph shows CS at 3 to 15% ESP & 5 to 25 % RHA

**Conclusions**

The research work has been carried out to examine the worth of RHA and ESP in oil and gas well cement as an additive to enhance compressive strength and rheological properties. The results showed that cement slurry mixed with RHA and ESP has better properties than base slurry, and following points are concluded out of this study:

1. Optimum results of CS are obtained with ESP between 8 to 10% and RHA between 10 to 15 %.
2. The best replacing level of locally manufactured cement with ESP and RHA is 10% each.
3. Maximum compressive strength of 31.32 MPa has been obtained with 10% ESP and 10% RHA in 72 hours of curing time.
4. At 72 hours curing periods and test conditions of 90°C temperature and 20 MPa pressure, cement appeared to have a better strength development compared to other curing periods of 08 and 24 hours.

5. Among all three variants of cement slurry minimum gel strength obtained is 6.2 lb/100 ft<sup>2</sup> with ESP0% & RHA0% and maximum gel obtained is 15.4 lb/100 ft<sup>2</sup> with ESP10 % and RHA10% at 10 sec.
6. The RHA has been a reliable option in replacement of silica flour (SF) in applications of oil well cementing. The RHA presented silica content above 90%, being similar to the commercial SF.
7. RHA and ESP have accelerating effect hence thickening time of slurry has been decreased with rise in concentration of both additives.
8. At test conditions of 90°C temperature and 20MPa pressure, no premature gelation of cement slurry has been noticed for all cement samples prepared from RHA and ESP.

**References**

Agofack, N., Ghabezloo, S., Sulem, J., Garnier, A., & Urbanczyk, C. (2019) Experimental investigation of the early-age mechanical behaviour of oil-well cement paste.

Ahmadi SA, Shakib JT, Ghaderi A, Beirami A (2013) The Performance of Foam Cement in Iran Oil Wells and Comparison of Bentonite Light Cement with Foam Cement and Presentation of Foam, Cement Advantages in Iran Oil Wells. Australian Journal of Basic and Applied Sciences 7: 696-702.

A. Lavrov and M. Torsæter (2016) Physics and Mechanics of Primary Well Cementing, SpringerBriefs in Petroleum Geoscience & Engineering, DOI 10.1007/978-3-319-43165-9\_2

Amarnath Yerramala., (2014), "Properties of Concrete with Eggshell Powder as Cement Replacement", The Indian Concrete Journal, PP 94-102

A. M. King'ori, "A Review of the uses of poultry eggshells and shell membranes," Int. J. Poult.Sci., vol. 10, no. 11, pp. 908-912, 2011.

API, "10A Specification for Cements and Materials for Well Cementing," 2010 (2019) A Review Study of Egg Shell Powder as a Cement Replacing Material in Concrete, (May), 5432-5436.

Benjamin I, Joe M, Daniel B (2010) Strength retrogression in cement under high temperatures. In: SGP- TR-188, unity fifth workshop on geothermal reservoir simulation. Stanford, California, pp 1-8

Bourgoyne (2000) a review of sustained casing pressure occurring on outer continental shelf, final report, mineral management services, USA.

Dave Duarte (2015) Cement Slurry with Silica Flour and Calcined Clay for Cementation of Oil-Wells Subject to High Temperature, Venezuela: Departamento de Ingeniería de Materiales, Universidad Simón Bolívar, Baruta-1086A.

Di Lullo, G. and Rae, P., Cements for Long Term Isolation - Design Optimization by Computer Modelling and Prediction, (2000) IADC/SPE 62745, Kuala Lumpur, Malaysia, Sep 11-13.

E.Barlet-Gouedard, Véronique Porcherie, Olivier Pershikova,(2009) "Pumpable geopolymer formulation for oilfield application," 08290157.0

Eric Broni-Bediak et al. (2016) Oil Well Cement Additives: Areview of the Common Types. Oil and Gas Research, 2016, Volume 2. Issue 2.

Erik B. Nelson and Dominique Guillot, Ed., (2006) Well Cementing, 2nd ed. Sugar Land, Texas 77478, US: Schlumberger

- Falode OA, Salam KK, Arinkoola AO, Ajagbe BM (2013) Prediction of Compressive Strength of Oil Field Class G Cement Slurry using Factorial Design. *Journal of Petroleum Exploration Production Technology* 3: 297-302.
- Habeeb, G.A. and H.B. Mahmud (2010) Study on Properties of Rice Husk Ash and Its Use as Cement Replacement Material. *Materials Research*, 13(2): 185-190
- Hakim Saaid Saleh (June 2016) *Proper Cementing to Reduce Time and Cost*, 1st edn., University of Stavanger.
- Herianto A, Fathaddin MT (2005) Effects of additives and conditioning time on comprehensive and shear bond strengths of geothermal well cement. In: *Proceedings of world geothermal congress*. Antalya, Turkey, pp 1-7
- Huwel J, Faustino V, Roberts R (2014) Crest Pumping Technologies Cement Compressive Strength Development Drastically Affected by Testing Procedure. *Proceedings of American Association of Drilling Engineers Fluid Conference and Exhibitionouston Texas* 1-5.
- Huwel JPE, Faustino V, Roberts R (2014) Cement Compressive Strength Development Drastically Affected by Testing Procedure. *Proceedings of American Association of Drilling Engineers Fluid Conference and Exhibition Houston Texas, USA*.
- Jafariesfad, N., Geiker, M. R., Gong, Y., Skalle, P., Zhang, Z., & He, J. (2017) Cement sheath modification using nanomaterials for long-term zonal isolation of oil wells: Review. *Journal of Petroleum Science and Engineering*, 156(June),662-672.
- Khan B, Ullah M (2004) Effect of a Retarding Admixture on the Setting Time of Cement Pastes in Hot Weather. *Journal of King Abdulaziz University Engineering Sciences* 15: 63-79.
- Koteswara Rao, D., P.R.T. Pranav and M. Anusha, 2012. Stabilization of Expansive Soil with Rice Husk Ash, Lime and Gypsum An Experimental Study. *International Journal of Engineering Science and Technology*, 3: 8076-8085.
- Kutasov IM, Eppelbaum LV (2014) Temperature Regime of Boreholes: Cementing of Production Liners *Proceedings of Thirty-Ninth Workshop on Geothermal Reservoir Engineering Stanford*. University Stanford California 1-5.
- Lavrov, A., & Torsæter, M. (2016) *Physics and Mechanics of Primary Well Cementing*.
- Labibzadeh M, Zahabizadeh B, Khajehdezfuly A (2010) Early-age Compressive Strength Assessment of Oil Well Class G Cement due to Borehole Pressure and Temperature Changes. *Journal of American Science* 6: 39-47.
- Loo, Y.C., P. Nimityongskul and P. Karasudhi (1984) Economical Rice Husk Ash Concrete. *Building, Research and Practice*, 12(4): 233-238.
- Margarini P, Lanzetta C, Galletta A (1999) *Drilling Design Manual Eni-Agip Division* 97-107.
- Mtallib M. O. A., Rabiou A., (2009), " Effect of Eggshells Ash on the Setting Time of Cement", *Nigerian Journal of Technology*, Volume 28, Issue 2, PP 29-38
- M.N.N. Khan et al, (2014) *Australian Journal of Basic and Applied Sciences*, 8(19) Special 2014, Pages: 176-181
- Ozyurtkan, M. Hakanet al. (2013) an experimental study on mitigation of oil well cement gas permeability. *International Petroleum Technology Conference*, 26-28 March, Beijing China.
- Pikłowska, A. (2017) Cement slurries used in drilling – types , properties , application, 76, 149-165.
- Raman, S.N., T. Ngo, P. Mendis and H.B. Mahmud (2011) High-Strength Rice Husk Ash Concrete Incorporating Quarry Dust as a Partial Substitute for Sand. *Construction and Building Materials*, 25: 3123-3130.
- Ramos, R. M., & Camus, A. S. (2017). Borehole Cement Sheath Integrity-Numerical Simulation Under Reservoir Conditions, XXXV, 7-10.
- Ridha S, Irawan S, Ariwahjoedi B (2013) Strength Prediction of Class G Oil Well Cement during Early Ages by Electrical Conductivity. *Journal of Petroleum Exploration Production Technology* 3: 303-311.
- Rike JL (1973) Obtaining Successful Squeeze Cement Result *Society of Petroleum Engineers SPE* 4608.
- Shadizadeh SR, Kholghi M, Kassaei MH (2010) Experimental Investigation of Silica Fume as a Cement Extender for Liner Cementing in Iranian Oil/Gas Wells. *Iranian Journal of Chemical Engineering* 7: 42-66.
- Shuker MT, Memon KR, Tunio SQ, Memon MK (2014) Laboratory Investigation on Performance of Cement Using Different Additives Schemes to Improve Early Age Compressive Strength Research. *Journal of Applied Sciences Engineering and Technology* 7: 2298-2305.
- Siddique, R., (2008) *Waste Materials and By-Products in Concrete with 174 Tables*. Springer Press.
- Slagle KA, Carter GL (1958) Gilsonite - A Unique Additive for Oil-well Cements *Spring Meeting of the Southern District Division of Production New Orleans* 318-328.
- Smith, R.G. and G.A. Kamwanja, (1986) The Use of Rice Husk for Making a Cementitious Material. In the *Proceeding of Joint Symposium on Use of Vegetable Plants and their Fibers as Building Material*, pp: 85-94.
- Soran Talabanic&GeirHareland (1995) new cement additive that eliminate cement body permeability. *International Petroleum Technology Conference*, 26-28 March, Beijing China.
- U.N. Okonkwo, I.C. Odiong, and E.E. Akpabio (2012)The effects of eggshell ash on strength properties of cement-stabilized lateric, *Int. J. of Sustainable Construction Engineering and Technology*, 13(1),18-25
- W. Renpu, (2011) *Advanced Well Completion Engineering*, 3rd ed. Gulf Professional Publishing
- Xi F, Qu J, Lv G, Tan W, Wang C (2010) Study of deep water cement experimental method and cement slurry. *International Offshore and Polar Engineering Conference Beijing, China*