

Research Article

EDM of Heat Treated-Al 7075

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Abstract

In this paper the electric discharge machining of heat treated AA-7075 were carried and tool wear rate was investigated. Pulse on-time, pulse off-time, servo voltage and peak current were the input process parameters. Experiments were conducted according to central composite design. Pulse on-time had the maximum contribution on tool wear rate followed by pulse off-time and servo voltage.

Keywords: EDM, AA 7075, CCD, TWR.

1. Introduction

Electrical Discharge Machine (EDM) is an electro-thermal non-traditional machining Process, where electrical energy is used to generate electrical spark and material removal mainly occurs due to thermal energy of the spark. Following paragraphs describe researches carried on EDM:

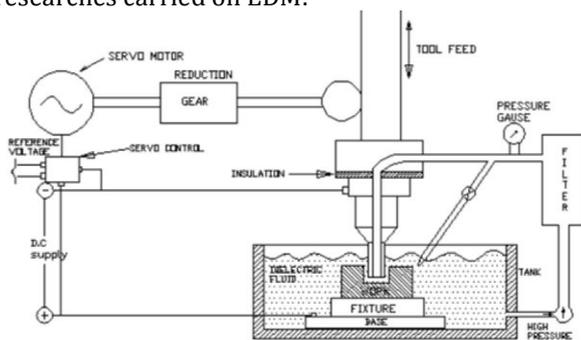


Figure 1: Working principle of EDM Process

Patel *et al.* (2009) developed ceramic composite material (Al₂O₃-SiCw-TiC) and selected to investigate its EDM machinability. The recent developments in ceramic composites are focused not only on the improvements of strength and toughness, but also on possibilities for difficult-to-machine shapes using EDM.

Yu *et al.* (2009) said that when a micro-hole is drilled deeply by EDM, the viscous resistance in the narrow discharge gap causes difficulty in the removal of debris and bubbles from the working area, leading to frequent occurrences of abnormal discharges and resulting in extensive electrode wear.

Chern *et al.* (2007) studied burr formation in micro-machining using micro-tools. The micro-tools

employed are fabricated by micro-EDM using the wire electro-discharge grinding (WEDG) method in the micro-EDM/milling machine we had already developed. Micro tungsten-carbide tool with a minimum of 31µm in diameter had been fabricated.

Abbas *et al.* (2006) analysed that Electrical discharge machining (EDM) is one of the earliest non-traditional machining processes. EDM process is based on thermoelectric energy between the work piece and an electrode. A pulse discharge occurs in a small gap between the work piece and the electrode and removes the unwanted material from the parent metal through melting and vaporising.

Guu and Hou (2007) analysed surface characteristics caused by EDM by means of the atomic force microscopy (AFM) technique. An empirical model of Fe-Mn-Al alloy was proposed based on the experimental data. A qualitative energy dispersive spectroscopic analyzer was used to measure the chemical composition of the specimen. Surface hardness was determined with a micro hardness tester.

Jeong and Min (2007) proposed Geometric simulation model of EDM drilling process with cylindrical tool to predict the geometries of tool and drilled hole. The geometries of tool and workpiece are represented by two dimensional matrixes. For accurate prediction of their geometries, the tool motion, the sparking gap width, the spark frequency, the crater made by a single spark, and the tool wear ratio are considered as simulation parameters.

Taweel (2008) studied relationship of process parameters in electro-discharge of CK45 steel with novel tool electrode material such as Al-Cu-Si-TiC composite produced using powder metallurgy (P/M) technique. The central composite second-order rotatable design had been utilized to plan the

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experiments, and response surface methodology (RSM) was employed for developing experimental models. Analysis on machining characteristics of electrical discharge machining (EDM) die sinking was made based on the developed models. In this study, titanium carbide percent (TiC%), peak current, dielectric flushing pressure, and pulse on-time are considered as input process parameters.

A number of researchers (Gupta et al., 2012; Sharma et al., 2011, 2013a; 2013b; 2014a; 2014b; 2014c; 2015; Kumar et al. (2014), Khanna et al., 2015) utilized planning of experimentation to reduce the experiments and analysis the process parameters. In the present research electric discharge machining of heat treated aero-space alloy AA 7075 was considered and metal removal rate was investigated.

Table 1: Process parameters, units and its Range

S.No.	Process Parameters	Notation	Unit	Range
1	Pulse on-time	Ton	μs	130-170
2	Pulse off-time	Toff	μs	30-45
3	Peak Current	IP	A	2-5
4	Servo voltage	SV	V	30-50

2. Experimentations

The experiments were carried out on EDM machine (ELEKTRA PLUS R50) of Electronica Machine Tools Ltd.

Design: Fixed column, moving table

Table size: 500 x 300 mm

Max. Height above the table: 250 mm

Max. permitted load on table: 175 kg

Max. electrode weight: 50 kg

Weight is measured by the Mitutoyo make high precision weight balance with least count 0.001g.

Tool wear rate was calculated by below mentioned formula

$$\text{Tool Wear rate} = (\text{Initial weight} - \text{Final Weight}) / (\text{Time taken})$$

The range of process parameters is given in Table 1.

2. Results and discussions

Table 2 represent the design matrix for four parameters and corresponding values of MRR. Experiments are performed according to run order.

Table 2: Design Matrix and Responses

Std	Run	A:Ton (us)	B:Toff (us)	C:IP (A)	D:SV (V)	MRR (mg/min)
5	1	170	30	2	50	0.0977
13	2	150	37.5	0.98	40	0.0559
16	3	150	37.5	3.5	56.82	0.0907
1	4	170	45	5	30	0.0669
9	5	116.36	37.5	3.5	40	0.0521
7	6	130	45	5	50	0.05293
17	7	150	37.5	3.5	40	0.0807
19	8	150	37.5	3.5	40	0.0865
3	9	170	30	5	50	0.0593
18	10	150	37.5	3.5	40	0.0881
21	11	150	37.5	3.5	40	0.0893
20	12	150	37.5	3.5	40	0.0879
4	13	130	45	2	50	0.0403
2	14	170	45	2	30	0.0863
12	15	150	50.11	3.5	40	0.0878
15	16	150	37.5	3.5	23.18	0.0623
8	17	130	30	2	30	0.0299
10	18	183.64	37.5	3.5	40	0.1171
6	19	130	30	5	30	0.0789
11	20	150	24.89	3.5	40	0.0311
14	21	150	37.5	6.02	40	0.0752

The analysis of response data is done by well-known software Design Expert specifically used for the design of experiment applications.

3.1 Analysis of Tool Wear Rate (TWR)

Table 3 shows the ANOVA for TWR during the experimentation of EDM. Quadratic model is significant

and lack of fit is non-significant. Pulse-on time, off-time and servo voltage are significant factors along with interaction and quadratic parameters of off-time, servo voltage and Peak current.

The Model F-value of 27.10 implies the model is significant. There is only a 0.01% chance that a Model F-Value this large could occur due to noise. Values of Prob > F less than 0.0500 indicate model terms are

Table 3 Analysis of Variance for TWR

Source	SS	df	MS	F-Value	p-value	
Model	0.01	14	7.33E-04	31.03	0.0002	significant
A-Ton	2.11E-03	1	2.11E-03	89.42	< 0.0001	
B-Toff	1.61E-03	1	1.61E-03	68.04	0.0002	
C-IP	9.64E-05	1	9.64E-05	4.08	0.0899	
D-SV	4.03E-04	1	4.03E-04	17.07	0.0061	
AB	3.26E-04	1	3.26E-04	13.79	0.0099	
AC	1.78E-03	1	1.78E-03	75.47	0.0001	
AD	1.23E-03	1	1.23E-03	52.13	0.0004	
BC	3.77E-05	1	3.77E-05	1.6	0.2533	
BD	1.12E-04	1	1.12E-04	4.72	0.0727	
CD	3.83E-04	1	3.83E-04	16.22	0.0069	
A^2	1.38E-05	1	1.38E-05	0.59	0.4733	
B^2	1.45E-03	1	1.45E-03	61.42	0.0002	
C^2	8.85E-04	1	8.85E-04	37.48	0.0009	
D^2	2.19E-04	1	2.19E-04	9.26	0.0227	
Residual	1.42E-04	6	2.36E-05			
Lack of Fit	9.57E-05	2	4.79E-05	4.16	0.1053	not significant
Pure Error	4.60E-05	4	1.15E-05			
Cor Total	0.01	20				

significant. In this case A, B, D, AB, AC, AD, CD, B2, C2, D2 are significant model terms. Values greater than 0.1000 indicate the model terms are not significant. If there are many insignificant model terms (not counting those required to support hierarchy), model reduction may improve your model. The Lack of Fit F-value of 4.50 implies there is a 8.50% chance that a Lack of Fit F-value this large could occur due to noise. Lack of fit is bad we want the model to fit. This relatively low probability (<10%) is troubling.

Figure 2 and Figure 3 represent the normal plot of residual and predicted vs actual. In both figures residuals falls on a straight line, which verifies the ANOVA test.

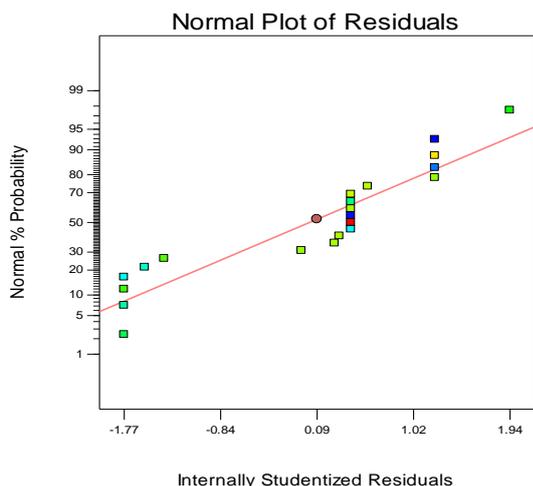


Figure 2: Normal Plot of Residuals (TWR)

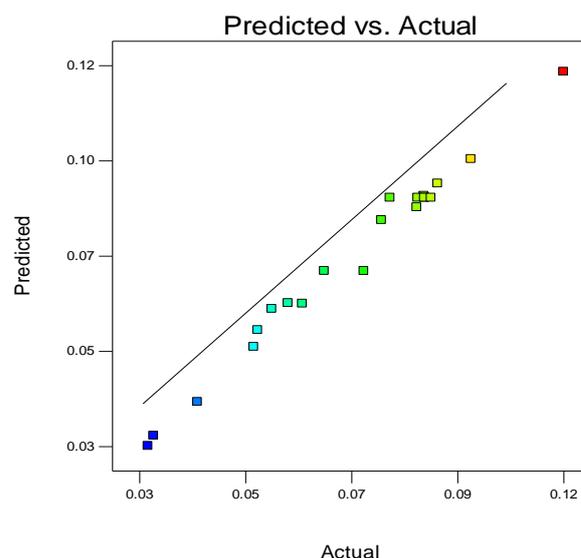


Figure 3: Predicted Vs Actual (TWR)

Table 4: Predicted optimal value of TWR

Responses	TWR
Optimized Setting	A ₁₃₀ B ₃₀ C ₃ D ₄₉
Predicted Value	0.0289
Actual Value	0.031

From Table 4 it is revealed that at optimized setting confirmations experiments present excellent results reproducibility.

Conclusions

Following Conclusion comes into picture after this research work

1. Tool wear rate increase with the increase of pulse on time and peak current.
2. TWR decreases with increase of pulse off time and servo-voltage.
3. A strong interaction between pulse-on time and peak current; pulse on time and servo voltage is observed.

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